- The IIR and FIR filter design techniques discussed so far can be easily implemented on a computer
- In addition, there are a number of filter design algorithms that rely on some type of optimization techniques that are used to minimize the error between the desired frequency response and that of the computer-generated filter

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- Basic idea behind the computer-based iterative technique
- Let H(e^{jω}) denote the frequency response of the digital filter H(z) to be designed approximating the desired frequency response D(e^{jω}), given as a piecewise linear function of ω, in some sense

- <u>Objective</u> Determine iteratively the coefficients of H(z) so that the difference between between $H(e^{j\omega})$ and $D(e^{j\omega})$ over closed subintervals of $0 \le \omega \le \pi$ is minimized
- This difference usually specified as a weighted error function

 $E(\omega) = W(e^{j\omega})[H(e^{j\omega}) - D(e^{j\omega})]$ where $W(e^{j\omega})$ is some user-specified weighting function

• Chebyshev or minimax criterion -Minimizes the peak absolute value of the weighted error:

 $\varepsilon = \max_{\omega \in R} |E(\omega)|$

where *R* is the set of disjoint frequency bands in the range $0 \le \omega \le \pi$, on which $D(e^{j\omega})$ is defined

• For example, for a lowpass filter design, *R* is the disjoint union of $[0, \omega_p]$ and $[\omega_s, \pi]$

• Least-p Criterion - Minimize

$$\varepsilon = \int |W(e^{j\omega})[H(e^{j\omega}) - D(e^{j\omega})]|^p d\omega$$

$$\omega \in \mathbb{R}$$

over the specified frequency range *R* with *p* a positive integer

- *p* = 2 yields the **least-squares criterion**
- As $p \to \infty$, the least *p*-th solution approaches the minimax solution

- Least-*p* Criterion In practice, the p-th power error measure is approximated as $\varepsilon = \sum_{i=1}^{K} \{W(e^{j\omega_i})[H(e^{j\omega_i}) - D(e^{j\omega_i})]\}^p$ where ω_i , $1 \le i \le K$, is a suitably chosen dense grid of digital angular frequencies
- For linear-phase FIR filter design, $H(e^{j\omega})$ and $D(e^{j\omega})$ are zero-phase frequency responses
- For IIR filter design, $H(e^{j\omega})$ and $D(e^{j\omega})$ are magnitude functions

• The linear-phase FIR filter obtained by minimizing the peak absolute value of

$$\varepsilon = \max_{\omega \in R} |\mathcal{E}(\omega)|$$

is usually called the equiripple FIR filter

• After ε is minimized, the weighted error function $E(\omega)$ exhibits an equiripple behavior in the frequency range *R*

• The general form of frequency response of a causal linear-phase FIR filter of length 2M+1:

$$H(e^{j\omega}) = e^{-jM\omega}e^{j\beta}\breve{H}(\omega)$$

where the amplitude response $\breve{H}(\omega)$ is a real function of ω

• Weighted error function is given by $E(\omega) = W(\omega)[\breve{H}(\omega) - D(\omega)]$ where $D(\omega)$ is the desired amplitude

response and $W(\omega)$ is a positive weighting function

- Parks-McClellan Algorithm Based on iteratively adjusting the coefficients of H(ω) until the peak absolute value of E(ω) is minimized
- If peak absolute value of $E(\omega)$ in a band $\omega_a \le \omega \le \omega_b$ is ε_o , then the absolute error satisfies

$$|\breve{H}(\omega) - D(\omega)| \le \frac{\varepsilon_o}{|W(\omega)|}, \quad \omega_a \le \omega \le \omega_b$$

• For filter design,

 $D(\omega) = \begin{cases} 1, & \text{in the passband} \\ 0, & \text{in the stopband} \end{cases}$

• $\breve{H}(\omega)$ is required to satisfy the above desired response with a ripple of $\pm \delta_p$ in the passband and a ripple of δ_s in the stopband

• Thus, weighting function can be chosen either as

$$W(\omega) = \begin{cases} 1, & \text{in the passband} \\ \delta_p / \delta_s, & \text{in the stopband} \end{cases}$$

or

 $W(\omega) = \begin{cases} \delta_s / \delta_p, & \text{in the passband} \\ 1, & \text{in the stopband} \end{cases}$

• **Type 1 FIR Filter** - $\breve{H}(\omega) = \sum_{k=0}^{m} a[k] \cos(\omega k)$ where

 $a[0] = h[M], a[k] = 2h[M - k], 1 \le k \le M$

• Type 2 FIR filter -

$$\widetilde{H}(\omega) = \sum_{k=1}^{(2M+1)/2} b[k] \cos\left(\omega(k-\frac{1}{2})\right)$$

where

$$b[k] = 2h[\frac{2M+1}{2}-k], \ 1 \le k \le \frac{2M+1}{2}$$

Design of Equiripple Linear-Phase FIR Filters • **Type 3 FIR Filter** - $\breve{H}(\omega) = \sum_{k=1}^{M} c[k] \sin(\omega k)$

where

 $c[k] = 2h[M-k], \ 1 \le k \le M$

• Type 4 FIR Filter - $\breve{H}(\omega) = \sum_{k=1}^{(2M+1)/2} d[k] \sin\left(\omega(k-\frac{1}{2})\right)$ where

$$d[k] = 2h[\frac{2M+1}{2} - k], \quad 1 \le k \le \frac{2M+1}{2}$$

• Amplitude response for all 4 types of linearphase FIR filters can be expressed as

 $\breve{H}(\omega) = Q(\omega)A(\omega)$

where

 $Q(\omega) = \begin{cases} 1, & \text{for Type 1} \\ \cos(\omega/2), & \text{for Type 2} \\ \sin(\omega), & \text{for Type 3} \\ \sin(\omega/2), & \text{for Type 4} \end{cases}$

$$\begin{array}{l} \text{Design of Equipple}\\ \text{Linear-Phase FIR Filters} \end{array}$$
and
$$A(\omega) = \sum_{k=0}^{L} \widetilde{a}[k] \cos(\omega k)$$
where
$$\widetilde{a}[k] = \begin{cases} a[k], & \text{for Type 1} \\ \widetilde{b}[k], & \text{for Type 2} \\ \widetilde{c}[k], & \text{for Type 3} \\ \widetilde{d}[k], & \text{for Type 4} \end{cases}$$

with

$$L = \begin{cases} M, & \text{for Type 1} \\ \frac{2M-1}{2}, & \text{for Type 2} \\ M-1, & \text{for Type 3} \\ \frac{2M-1}{2}, & \text{for Type 4} \end{cases}$$

 $\tilde{b}[k]$, $\tilde{c}[k]$, and $\tilde{d}[k]$, are related to b[k], c[k], and d[k], respectively

 Modified form of weighted error function $E(\omega) = W(\omega)[Q(\omega)A(\omega) - D(\omega)]$ $= W(\omega)Q(\omega)[A(\omega) - \frac{D(\omega)}{O(\omega)}]$ $= \widetilde{W}(\omega) [A(\omega) - \widetilde{D}(\omega)]$ where we have used the notation $\widetilde{W}(\omega) = W(\omega)O(\omega)$ $\widetilde{D}(\omega) = D(\omega) / Q(\omega)$

• <u>Optimization Problem</u> - Determine $\tilde{a}[k]$ which minimize the peak absolute value ε of $E(\omega) = \tilde{W}(\omega) [\sum_{k=0}^{L} \tilde{a}[k] \cos(\omega k) - \tilde{D}(\omega)]$

over the specified frequency bands $\omega \in R$

 After ã[k] has been determined, corresponding coefficients of the original A(e^{jω}) are computed from which h[n] are determined

• Alternation Theorem - $A(\omega)$ is the best unique approximation of $D(\omega)$ obtained by minimizing peak absolute value ε of $E(\omega) = W(\omega)[Q(\omega)A(\omega) - D(\omega)]$ if and only if there exist at least L+2extremal frequencies, $\{\omega_i\}, 0 \le i \le L+1$, in a closed subset R of the frequency range $0 \le \omega \le \pi$ such that $\omega_0 < \omega_1 < \cdots < \omega_L < \omega_{L+1}$ and $E(\omega_i) = -E(\omega_{i+1})$, $|E(\omega_i)| = \varepsilon$ for all *i* Copyright © 2001, S. K. Mitra

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- Consider a Type 1 FIR filter with an amplitude response A(ω) whose approximation error E(ω) satisfies the Alternation Theorem
- Peaks of $E(\omega)$ are at $\omega = \omega_i$, $0 \le i \le L+1$ where $dE(\omega)/d\omega = 0$
- Since in the passband and stopband, $\widetilde{W}(\omega)$ and $\widetilde{D}(\omega)$ are piecewise constant, $\frac{dE(\omega)}{d\omega} = \frac{dA(\omega)}{d\omega} = 0 \text{ at } \omega = \omega_i$

- Using $\cos(\omega k) = T_k(\cos \omega)$, where $T_k(x)$ is the *k*-th order Chebyshev polynomial $T_k(x) = \cos(k \cos^{-1} x)$
- $A(\omega)$ can be expressed as $A(\omega) = \sum_{k=0}^{L} \alpha[k] (\cos \omega)^k$

which is an *L*th-order polynomial in $\cos \omega$

 Hence, A(ω) can have at most L-1 local minima and maxima inside specified passband and stopband

- At bandedges, $\omega = \omega_p$ and $\omega = \omega_s$, $|E(\omega)|$ is a maximum, and hence $A(\omega)$ has extrema at these points
- $A(\omega)$ can have extrema at $\omega = 0$ and $\omega = \pi$
- Therefore, there are at most L+3 extremal frequencies of E(ω)
- For linear-phase FIR filters with *K* specified bandedges, there can be at most *L*+*K*+1 extremal frequencies

• The set of equations $\widetilde{W}(\omega_i)[A(\omega_i) - \widetilde{D}(\omega_i)] = (-1)^i \varepsilon, \ 0 \le i \le L+1$ is written in a matrix form $\cos(\omega_0) \cdots \cos(L\omega_0) - 1/\widetilde{W}(\omega_0) \quad \widetilde{a}[0] \quad \widetilde{D}(\omega_0)$

 $\begin{bmatrix} 1 & \cos(\omega_0) & \cdots & \cos(L\omega_0) & -1/\widetilde{W}(\omega_0) \\ 1 & \cos(\omega_1) & \cdots & \cos(L\omega_1) & 1/\widetilde{W}(\omega_1) \\ \vdots & \vdots & \ddots & \vdots & & \vdots \\ 1 & \cos(\omega_L) & \cdots & \cos(L\omega_L) & (-1)^{L-1}/\widetilde{W}(\omega_L) \\ 1 & \cos(\omega_{L+1}) & \cdots & \cos(L\omega_{L+1}) & (-1)^L/\widetilde{W}(\omega_{L+1}) \end{bmatrix} \begin{bmatrix} \widetilde{a}[0] \\ \widetilde{a}[1] \\ \vdots \\ \widetilde{a}[L] \\ \varepsilon \end{bmatrix} = \begin{bmatrix} \widetilde{D}(\omega_0) \\ \widetilde{D}(\omega_1) \\ \vdots \\ \widetilde{D}(\omega_L) \\ \widetilde{D}(\omega_L) \\ \widetilde{D}(\omega_{L+1}) \end{bmatrix}$

- The matrix equation can be solved for the unknowns ã[i] and ε if the locations of the L+2 extremal frequencies are known a priori
- The **Remez exchange algorithm** is used to determine the locations of the extremal frequencies

• <u>Step 1</u>: A set of initial values of extremal frequencies are either chosen or are available from completion of previous stage

• Step 2: Value of
$$\varepsilon$$
 is computed using
 $\varepsilon = \frac{c_0 \widetilde{D}(\omega_0) + c_1 \widetilde{D}(\omega_1) + \dots + c_{L+1} \widetilde{D}(\omega_{L+1})}{\widetilde{W}(\omega_0)} - \frac{c_1}{\widetilde{W}(\omega_1)} + \dots + \frac{(-1)^{L+1} c_{L+1}}{\widetilde{W}(\omega_{L+1})}$
where $c_n = \prod_{\substack{i=0\\i\neq n}}^{L+1} \frac{1}{\cos(\omega_n) - \cos(\omega_i)}$

• <u>Step 3</u>: Values of $A(\omega)$ at $\omega = \omega_i$ are then computed using

$$A(\omega_i) = \frac{(-1)^i \varepsilon}{\widetilde{W}(\omega_i)} + \widetilde{D}(\omega_i), \quad 0 \le i \le L+1$$

 <u>Step 4</u>: The polynomial A(ω) is determined by interpolating the above values at the L+2 extremal frequencies using the Lagrange interpolation formula

• <u>Step 4</u>: The new error function

$$E(\omega) = \tilde{W}(\omega)[A(\omega) - \tilde{D}(\omega)]$$

is computed at a dense set $S (S \ge L)$ of frequencies. In practice S = 16L is adequate. Determine the L+2 new extremal frequencies from the values of $E(\omega)$ evaluated at the dense set of frequencies.

<u>Step 5</u>: If the peak values ε of E(ω) are equal in magnitude, algorithm has converged. Otherwise, go back to Step 2.

• Illustration of algorithm



Iteration process is stopped if the difference between the values of the peak absolute errors between two consecutive stages is less than a preset value, e.g., 10^{-6}

• Example - Approximate the desired function $D(x) = 1.1x^2 - 0.1$ defined for the range $0 \le x \le 2$ by a linear function $a_1x + a_0$ by minimizing the peak value of the absolute error

$$\max_{x \in [0,2]} \left| 1.1x^2 - 0.1 - a_0 - a_1 x \right|$$

• <u>Stage 1</u>:

Choose arbitrarily the initial extremal points $x_1 = 0, x_2 = 0.5, x_3 = 1.5$

• Solve the three linear equations $a_0 + a_1 x_{\ell} - (-1)^{\ell} \varepsilon = D(x_{\ell}), \quad \ell = 1, 2, 3$

i.e.,
$$\begin{bmatrix} 1 & 0 & 1 \\ 1 & 0.5 & -1 \\ 1 & 1.5 & 1 \end{bmatrix} \begin{bmatrix} a_0 \\ a_1 \\ \varepsilon \end{bmatrix} = \begin{bmatrix} -0.1 \\ 0.175 \\ 2.375 \end{bmatrix}$$

for the given extremal points yielding $a_0 = -0.375, a_1 = 1.65, \varepsilon = 0.275$

• Plot of $\mathcal{E}_1(x) = 1.1x^2 - 1.65x + 0.275$ along with values of error at chosen extremal points shown below



• Note: Errors are equal in magnitude and alternate in sign

- <u>Stage 2</u>:
- Choose extremal points where $\mathcal{F}_1(x)$ assumes its maximum absolute values
- These are $x_1 = 0, x_2 = 0.75, x_3 = 2$
- New values of unknowns are obtained by solving $\begin{bmatrix}
 1 & 0 & 1 \\
 1 & 0.75 & -1 \\
 1 & 2 & 1
 \end{bmatrix}
 \begin{bmatrix}
 a_0 \\
 a_1 \\
 \varepsilon
 \end{bmatrix} =
 \begin{bmatrix}
 -0.1 \\
 0.5188 \\
 4.3
 \end{bmatrix}$
 - yielding $a_0 = -0.6156, a_1 = 2.2, \varepsilon = 0.5156$

• Plot of $\mathcal{E}_2(x) = 1.1x^2 - 2.2x + 0.5156$ along with values of error at chosen extremal points shown below



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- <u>Stage 3</u>:
- Choose extremal points where $\mathcal{F}_2(x)$ assumes its maximum absolute values
- These are $x_1 = 0, x_2 = 1, x_3 = 2$
- New values of unknowns are obtained by solving $\begin{bmatrix} 1 & 0 & 1 \\ 1 & 1 & -1 \end{bmatrix} \begin{bmatrix} a_0 \\ a_1 \end{bmatrix} = \begin{bmatrix} -0.1 \\ 1.0 \end{bmatrix}$

$$\begin{bmatrix} 1 & 1 & 1 \\ 1 & 2 & 1 \end{bmatrix} \begin{bmatrix} a_1 \\ \varepsilon \end{bmatrix} \begin{bmatrix} a_1 \\ 4.3 \end{bmatrix}$$

yielding $a_0 = -0.65, a_1 = 2.2, \varepsilon = 0.55$

• Plot of $\mathcal{E}_3(x) = 1.1x^2 - 2.2x + 0.55$ along with values of error at chosen extremal points shown below



• Algorithm has converged as ε is also the maximum value of the absolute error

IIR Digital Filter Design Using MATLAB

- Order Estimation -
- For IIR filter design using bilinear transformation, MATLAB statements to determine the order and bandedge are: [N, Wn] = buttord(Wp, Ws, Rp, Rs);[N, Wn] = cheb1ord(Wp, Ws, Rp, Rs); [N, Wn] = cheb2ord(Wp, Ws, Rp, Rs);[N, Wn] = ellipord(Wp, Ws, Rp, Rs);
• <u>Example</u> - Determine the minimum order of a Type 2 Chebyshev digital highpass filter with the following specifications:

$$F_p = 1$$
 kHz, $F_p = 1$ kHz, $F_T = 4$ kHz,
 $\alpha_p = 1$ dB, $\alpha_s = 40$ dB

- Here, $Wp = 2 \times 1/4 = 0.5$, $Ws = 2 \times 0.6/4 = 0.3$
- Using the statement

 [N, Wn] = cheb2ord(0.5, 0.3, 1, 40);
 we get N = 5 and Wn = 0.3224

- Filter Design -
- For IIR filter design using bilinear transformation, MATLAB statements to use are:

• The form of transfer function obtained is

$$G(z) = \frac{B(z)}{A(z)} = \frac{b(1) + b(2)z^{-1} + \dots + b(N+1)z^{-N}}{1 + a(2)z^{-1} + \dots + a(N+1)z^{-N}}$$

- The frequency response can be computed using the M-file freqz(b, a, w) where w is a set of specified angular frequencies
- It generates a set of complex frequency response samples from which magnitude and/or phase response samples cn be computed

- Example Design an elliptic IIR lowpass filter with the specifications: $F_p = 0.8$ kHz, $F_s = 1$ kHz, $F_T = 4$ kHz, $\alpha_p = 0.5$ dB, $\alpha_s = 40$ dB
- Here, $\omega_p = 2\pi F_p / F_T = 0.4\pi, \omega_s = 2\pi F_s / F_T = 0.5\pi$
- Code fragments used are:
 [N,Wn] = ellipord(0.4, 0.5, 0.5, 40);
 [b, a] = ellip(N, 0.5, 40, Wn);

• Gain response plot is shown below:



- Order Estimation -
- Kaiser's Formula:

$$N \cong \frac{-20\log_{10}(\sqrt{\delta_p \delta_s})}{14.6(\omega_s - \omega_p)/2\pi}$$

• <u>Note</u>: Filter order *N* is inversely proportional to transition band width $(\omega_s - \omega_p)$ and does not depend on actual location of transition band

• Hermann-Rabiner-Chan's Formula:

$$N \cong \frac{D_{\infty}(\delta_p, \delta_s) - F(\delta_p, \delta_s) [(\omega_s - \omega_p)/2\pi]^2}{(\omega_s - \omega_p)/2\pi}$$

where

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$$D_{\infty}(\delta_{p}, \delta_{s}) = [a_{1}(\log_{10} \delta_{p})^{2} + a_{2}(\log_{10} \delta_{p}) + a_{3}]\log_{10} \delta_{s} + [a_{4}(\log_{10} \delta_{p})^{2} + a_{5}(\log_{10} \delta_{p}) + a_{6}]$$

$$F(\delta_{p}, \delta_{s}) = b_{1} + b_{2}[\log_{10} \delta_{p} - \log_{10} \delta_{s}]$$
with $a_{1} = 0.005309, a_{2} = 0.07114, a_{3} = -0.4761$
 $a_{4} = 0.00266, a_{5} = 0.5941, a_{6} = 0.4278$
 $b_{1} = 11.01217, b_{2} = 0.51244$

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- Formula valid for $\delta_p \ge \delta_s$
- For $\delta_p < \delta_s$, formula to be used is obtained by interchanging δ_p and δ_s
- Both formulas provide only an estimate of the required filter order *N*
- Frequency response of FIR filter designed using this estimated order may or may not meet the given specifications
- If specifications are not met, increase filter order until they are met

- MATLAB code fragments for estimating filter order using Kaiser's formula num = 20*log10(sqrt(dp*ds)) 13; den = 14.6*(Fs Fp)/FT; N = ceil(num/den);
- M-file remezord implements Hermann-Rabiner-Chan's order estimation formula

- For FIR filter design using the Kaiser window, window order is estimated using the M-file kaiserord
- The M-file kaiserord can in some cases generate a value of *N* which is either greater or smaller than the required minimum order
- If filter designed using the estimated order *N* does not meet the specifications, *N* should either be gradually increased or decreased until the specifications are met

- The M-file remez can be used to design an equiripple FIR filter using the Parks-McClellan algorithm
- Example Design an equiripple FIR filter with the specifications: $F_p = 0.8$ kHz, $F_s = 1$ kHz, $F_T = 4$ kHz, $\alpha_p = 0.5$ dB, $\alpha_s = 40$ dB
- Here, $\delta_p = 0.0559$ and $\delta_s = 0.01$

• MATLAB code fragments used are [N, fpts, mag, wt] =remezord(fedge, mval, dev, FT); b = remez(N, fpts, mag, wt);where fedge = $[800 \ 1000]$, $mval = \begin{bmatrix} 1 & 0 \end{bmatrix}, dev = \begin{bmatrix} 0.0559 & 0.01 \end{bmatrix}, and$ FT = 4000

- The computed gain response with the filter order obtained (N = 28) does not meet the specifications ($\alpha_p = 0.6$ dB, $\alpha_s = 38.7$ dB)
- Specifications are met with N = 30

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- <u>Example</u> Design a linear-phase FIR bandpass filter of order 26 with a passband from 0.3 to 0.5, and stopbands from 0 to 0.25 and from 0.55 to 1
- The pertinent input data here are N = 26
 - fpts = $\begin{bmatrix} 0 & 0.25 & 0.3 & 0.5 & 0.55 & 1 \end{bmatrix}$ mag = $\begin{bmatrix} 0 & 0 & 1 & 1 & 0 & 0 \end{bmatrix}$ wt = $\begin{bmatrix} 1 & 1 & 1 \end{bmatrix}$

• Computed gain response shown below where $\alpha_p = 1 \text{ dB}, \alpha_s = 18.7 \text{ dB}$



- We redesign the filter with order increased to 110
- Computed gain response shown below where $\alpha_p = 0.024 \text{ dB}, \alpha_s = 51.2 \text{ dB}$
- Note: Increase in order improves gain response at the expense of increased computational complexity



- α_s can be increased at the expenses of a larger α_p by decreasing the relative weight ratio $W(\omega) = \delta_p / \delta_s$ N = 110, weight ratio = 1/10
- Gain response of bandpass filter of order 110 obtained with a weight vector [1 0.1 1]



• Now $\alpha_p = 0.076 \, \text{dB}$, $\alpha_s = 60.86 \, \text{dB}$

0.2

0.1

0

0.1 Absolute Error 0.1 0.1 0.1

- Plots of absolute error for 1st design
- Absolute error has same peak value in all bands
- As L = 13, and there -0.2 0.2 0.4 0.6 ω/π are 4 band edges, there can be at most L - 1 + 6 = 18 extrema
- Error plot exhibits 17 extrema

0.8

N = 26, weight ratio = 1

- Absolute error has same peak value in all bands for the 2nd design
- Absolute error in passband of 3rd design is 10 times the error in the stopbands



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- <u>Example</u> Design a linear-phase FIR bandpass filter of order 60 with a passband from 0.3 to 0.5, and stopbands from 0 to 0.25 and from 0.6 to 1 with unequal weights
- The pertinent input data here are N = 60
 fpts = [0 0.25 0.3 0.5 0.6 1]
 mag = [0 0 1 1 0 0]
 wt = [1 1 0.3]

• Plots of gain response and absolute error shown below



- Response in the second transition band shows a peak with a value higher than that in passband
- Result does not contradict alternation theorem
- As N = 60, M = 30, and hence, there must be at least M + 2 = 32 extremal frequencies
- Plot of absolute error shows the presence of 32 extremal frequencies

- If gain response of filter designed exhibits a nonmonotonic behavior, it is recommended that either the filter order or the bandedges or the weighting function be adjusted until a satisfactory gain response has been obtained
- Gain plot obtained by moving the second stopband edge to 0.55



• A lowpass differentiator has a bandlimited frequency response

$$H_{DIF}(e^{j\omega}) = \begin{cases} j\omega, & 0 \le |\omega| \le \omega_p \\ 0, & \omega_s \le |\omega| \le \pi \end{cases}$$

where $0 \le |\omega| \le \omega_p$ represents the passband and $\omega_s \le |\omega| \le \pi$ represents the stopband

• For the design phase we choose $P(\omega) = 1/\omega, \quad D(\omega) = 1, \quad 0 \le |\omega| \le \omega_p$

- The M-file remezord cannot be used to estimate the order of an FIR differentiator
- <u>Example</u> Design a full-band $(\omega_p = \pi)$ differentiator of order 11
- Code fragment to use b = remez(N, fpts, mag, 'differentiator');where N = 11 $fpts = [0 \ 1]$ $mag = [0 \ pi]$

• Plots of magnitude response and absolute

error



• Absolute error increases with ω as the algorithm results in an equiripple error of the function $\left[\frac{A(\omega)}{\omega} - 1\right]$

- Example Design a lowpass differentiator of order 50 with $\omega_p = 0.4\pi$ and $\omega_s = 0.45\pi$
- Code fragment to use
 b = remez(N, fpts, mag, 'differentiator');
 where

N = 50fpts = [0 0.4 0.45 1] mag = [0 0.4*pi 0 0]

• Plot of the magnitude response of the lowpass differentiator



Equiripple FIR Hilbert Transformer Design Using MATLAB

• Desired amplitude response of a bandpass Hilbert transformer is

 $D(\omega) = 1, \quad \omega_L \le |\omega| \le \omega_H$

with weighting function

 $P(\omega) = 1, \quad \omega_L \le |\omega| \le \omega_H$

• Impulse response of an ideal Hilbert transformer satisfies the condition $h_{HT}[n] = 0$, for *n* even which can be met by a Type 3 FIR filter

Equiripple FIR Hilbert Transformer Design Using MATLAB

- Example Design a linear-phase bandpass FIR Hilbert transformer of order 20 with $\omega_L = 0.1\pi$, $\omega_H = 0.9\pi$
- Code fragment to use
 b = remez(N, fpts, mag, 'Hilbert');
 where

N = 20fpts = [0.1 0.9] mag = [1 1]

Equiripple FIR Hilbert Transformer Design Using MATLAB

• Plots of magnitude response and absolute error



• Window Generation - Code fragments to use w = blackman(L);w = hamming(L);w = hanning(L);w = chebwin(L, Rs);w = kaiser(L, beta);where window length L is odd

- <u>Example</u> Kaiser window design for use in a lowpass FIR filter design
- Specifications of lowpass filter: $\omega_p = 0.3\pi$, $\omega_s = 0.4\pi$, $\alpha_s = 50$ dB $\Rightarrow \delta_s = 0.003162$
- Code fragments to use

 [N, Wn, beta, ftype] = kaiserord(fpts, mag,dev);
 w = kaiser(N+1, beta);

 where fpts = [0.3 0.4]

 mag = [1 0]
 dev = [0.003162 0.003162]

• Plot of the gain response of the Kaiser window



- M-files available are fir1 and fir2
- fir1 is used to design conventional lowpass, highpass, bandpass, bandstop and multiband FIR filters
- **fir2** is used to design FIR filters with arbitrarily shaped magnitude response
- In fir1, Hamming window is used as a default if no window is specified

- Example Design using a Kaiser window a lowpass FIR filter with the specifications: $\omega_p = 0.3\pi, \omega_s = 0.4\pi, \delta_s = 0.003162$
- Code fragments to use

 [N, Wn, beta, ftype] = kaiserord(fpts, mag, dev);
 b = fir1(N, Wn, kaiser(N+1, beta));

 where fpts = [0.3 0.4]

 mag = [1 0]
 dev = [0.003162 0.003162]
• Plot of gain response



- Example Design using a Kaiser window a highpass FIR filter with the specifications: $\omega_p = 0.55\pi$, $\omega_s = 0.4\pi$, $\delta_s = 0.02$
- Code fragments to use
- [N, Wn, beta, ftype] = kaiserord(fpts, mag, dev);
 b = fir1(N, Wn, 'ftype', kaiser(N+1, beta));
 where fpts = [0.4 0.55] mag = [0 1] dev = [0.02 0.02]

• Plot of gain response



Example - Design using a Hamming window an FIR filter of order 100 with three different constant magnitude levels: 0.3 in the frequency range [0, 0.28], 1.0 in the frequency range [0.3, 0.5], and 0.7 in the frequency range [0.52, 1.0]

- Code fragment to use
 - b = fir2(100, fpts, mval);

where fpts = $[0 \ 0.28 \ 0.3 \ 0.5 \ 0.52 \ 1];$

mval = [0.3 0.3 1.0 1.0 0.7 0.7];

