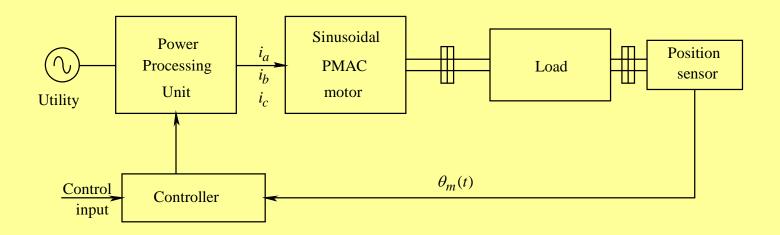
Sinusoidal Permanent Magnet AC (PMAC) Drives

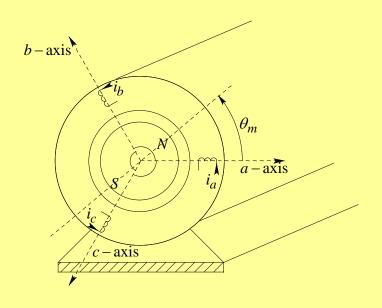
- ◆ Block Diagram
- ◆ Structure of Permanent-Magnet Synchronous Machines
- Principle of Operation
- ◆ Torque Calculation
- ◆ Similarity Between DC Motor and Brushless DC Motor
- ◆ Mechanical System
- ◆ Calculation of the Reference Current Values

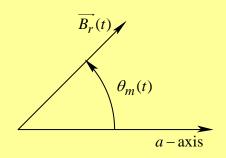
Permanent-Magnet AC (PMAC) Drives



- ☐ System level operation similar to DC machines but without brushes sometimes called Brush-less DC Drives
- ☐ Motor essentially a synchronous machine whose field flux is provided by permanent magnets

Structure of Permanent-Magnet Synchronous Machines





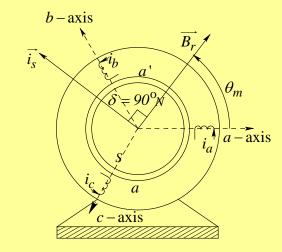
- ☐ Permanent Magnet rotor
- ☐ Sinusoidally distributed stator windings

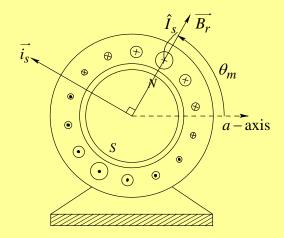
Principle of Operation

☐ Magnets shaped to produce sinusoidal flux density distribution

$$\overrightarrow{B_r}(t) = \hat{B}_r \angle \theta_m(t)$$

- ☐ Controlled stator currents
 - $\vec{i}_s(t)$ controlled by PPU (controlling $i_a(t)$, $i_b(t)$, and $i_c(t)$) such that $\vec{i}_s(t) = \hat{I}_s(t) \angle \theta_{i_s}(t), \text{ where}$ $\theta_{i_s}(t) = \theta_m(t) + 90^0$
 - $\delta = 90^{\circ}$ maximizes torque/ampere
 - Stator current space vector is controlled so that it leads the peak rotor flux by 90 degrees

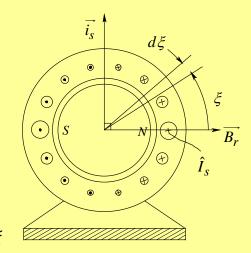




Torque Calculation

Using $f_{em} = Bli$

$$dT_{em}(\xi) = r \quad \hat{B}_r \cos \xi \quad \underbrace{\ell}_{flux \ density \ at \ \xi} \quad \underbrace{\ell}_{cond. length} \cdot \hat{I}_s \cdot \underbrace{\frac{N_s}{2} \cos \xi \cdot d\xi}_{diff \ no. of \ cond. at \ \xi}$$

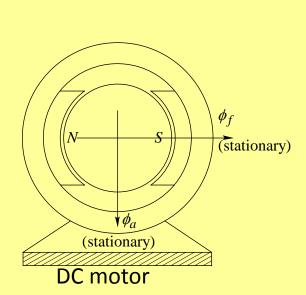


$$T_{em} = 2 \times \int_{\xi = -\pi/2}^{\xi = \pi/2} dT_{em}(\xi) = 2 \frac{N_s}{2} r \ell \hat{B}_r \hat{I}_s \int_{-\pi/2}^{\pi/2} \cos^2 \xi \cdot d\xi = \left[\pi \frac{N_s}{2} r \ell \hat{B}_r \right] \hat{I}_s$$

$$\Rightarrow T_{em} = k_{\tau} \hat{I}_{s}$$
, where the machine torque constant, $k_{T} = \pi \frac{N_{s}}{2} r \ell \hat{B}_{r}$

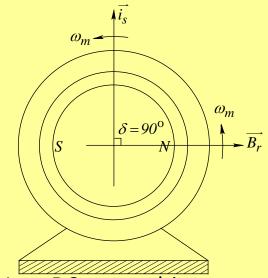
 \square Torque is proportional to \hat{I}_s alone, just as in dc motors with constant field excitation. Hence the name Brush-Less DC

Similarity Between DC Motor and Brushless DC Motor



• Stationary ϕ_f produced by stator windings

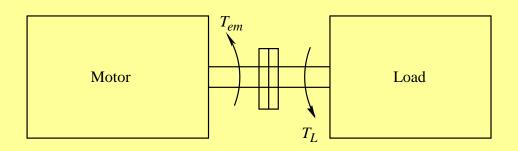
• ϕ_a produced by rotating rotor windings and is made stationary by commutator action



Brush-Less DC motor drive

- $\overrightarrow{B_r}$ produced by rotor magnets and rotates with the rotor
- $\vec{i_s}$ produced by stator winding currents and is made to rotate at rotor speed by the action of the PPU

Mechanical System



$$\alpha_m = \frac{d\omega_m}{dt} = \frac{T_{em} - T_L}{J_{eq}}$$

$$\omega_m(t) = \omega_m(0) + \int_0^t \alpha_m(\tau) \cdot d\tau$$

$$\theta_m(t) = \theta_m(0) + \int_0^t \omega_m(\tau) \cdot d\tau$$

Calculation of the Reference

Values: i_a^* , i_b^* and i_c^*

- ☐ Reference values are generated by the controller based on desired torque output and rotor position
- ☐ Reference values tell the PPU what stator currents to deliver
- ☐ Starting with the desired torque and known rotor position, the desired stator currents are found as follows:

$$(T_{em}^*, \theta_m) \rightarrow (\overrightarrow{i_s}) \rightarrow (\overrightarrow{i_a}, \overrightarrow{i_b}, \overrightarrow{i_c})$$

$$\hat{I}_{s}^{*}(t) = \frac{T_{em}^{*}(t)}{k_{T}}$$

$$i_{a}^{*}(t) = \frac{2}{3}\operatorname{Re}\left[\vec{i}_{s}^{*}(t)\right] = \frac{2}{3}\hat{I}_{s}^{*}(t)\cos\theta_{i_{s}}^{*}(t)$$

$$\theta_{i_{s}}^{*}(t) = \theta_{m}(t) + 90^{0}$$

$$i_{b}^{*}(t) = \frac{2}{3}\operatorname{Re}\left[\vec{i}_{s}^{*}(t)\angle - 120^{0}\right] = \frac{2}{3}\hat{I}_{s}^{*}(t)\cos(\theta_{i_{s}}^{*}(t) - 120^{0})$$

$$\vec{i}_{s}^{*}(t) = \hat{I}_{s}^{*}(t)\angle\theta_{i_{s}}^{*}(t)$$

$$i_{c}^{*}(t) = \frac{2}{3}\operatorname{Re}\left[\vec{i}_{s}^{*}(t)\angle - 240^{0}\right] = \frac{2}{3}\hat{I}_{s}^{*}(t)\cos(\theta_{i_{s}}^{*}(t) - 240^{0})$$

Example

 $k_{\tau} = 0.5 \text{ Nm/A}$ To produce a counter clockwise holding torque of 5 Nm at

$$\theta_m = 45^{\circ}$$

$$i_s$$
 i_b
 i_{a}
 i_{a}
 i_{a}
 i_{a}
 i_{a}
 i_{a}

$$\hat{I}_s = \frac{T_{em}}{k_T} = 10 A$$

$$\theta_{i_s} = \theta_m + 90^0 = 135^0$$

$$\vec{i}_s = \hat{I}_s \angle \theta_{i_s} = 10 \angle 135^0$$

$$i_a = \frac{2}{3}\hat{I}_s \cos\theta_{i_s} = -4.71 A$$

$$i_a = \frac{2}{3}\hat{I}_s\cos\theta_{i_s} = -4.71 A$$
 $i_b = \frac{2}{3}\hat{I}_s\cos(\theta_{i_s} - 120^0) = 6.44 A$

$$i_c = \frac{2}{3}\hat{I}_s \cos(\theta_{i_s} - 240^0) = -1.73 \text{ A}$$

Stator currents are dc in this example.

Summary

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